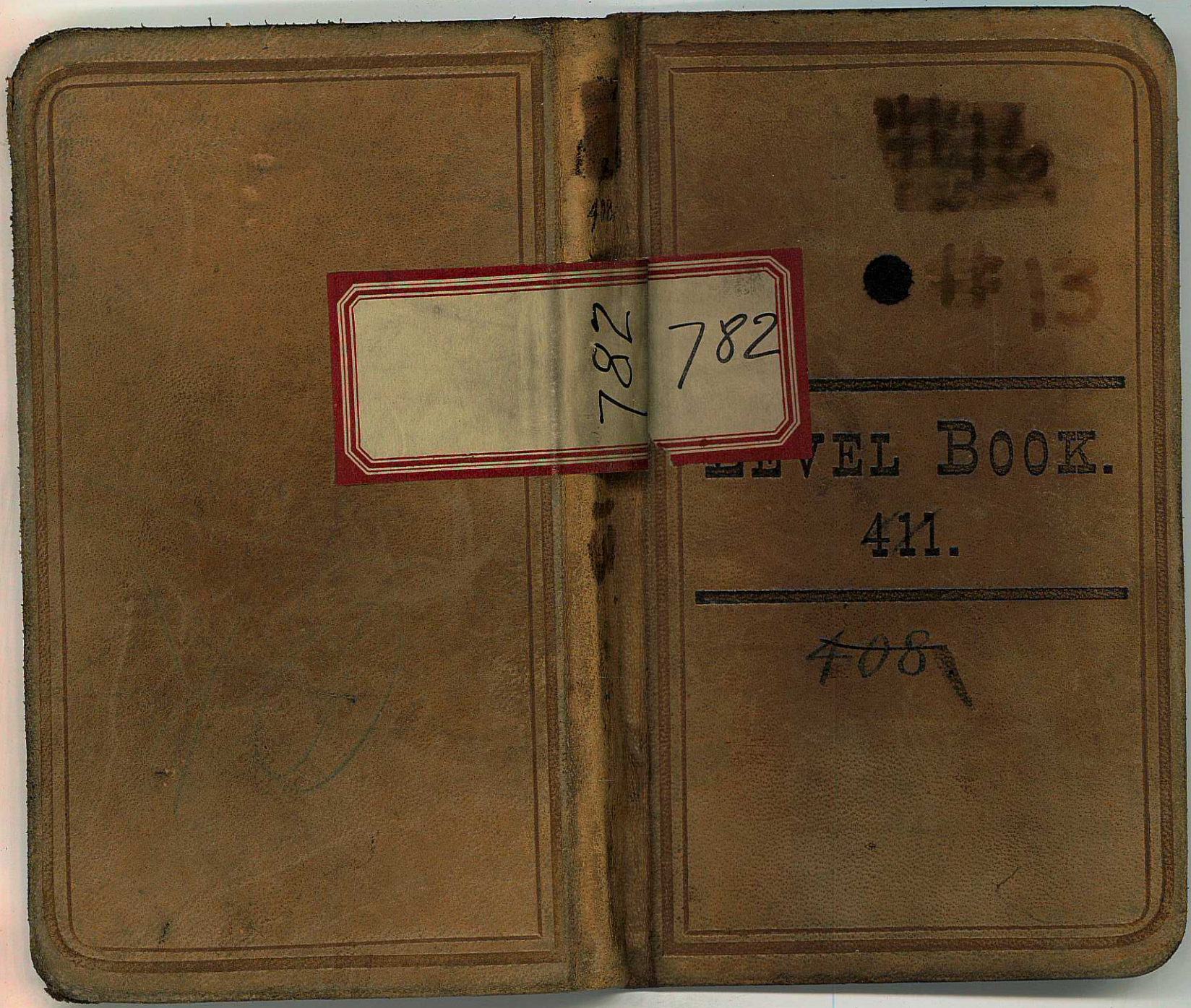

782
782
LEVEL BOOK.
411.
408

14 8
2.
10.

3 8 1
7 5 3
10 5 2
3 8 1
57.53

4.39

5 2 0 2
4 9 7 5
5

4975
15
74640

14

14/4 3

3 1/2

1 3 7 6 0
4 9 4 2
6 3 9 0 6 0
3.42
6 6 4 8

50 (11) 2
4

1.00087 10. ab
.00870 59

Equipment Schaub

Oct 1/04

5.77
.25
5.52
4
5.48

63.70
7 5 0
6 5 0
7 5 2 0 0

5.04
4.39
.65
2
1.30.

1.100 1.30 ✓

29 57 2

1001

63.82
16.50
9 3 2

501
.001 63.82
16.50
63.985

7876
6398.70
147750

1 Grade for J. E Wilson
on N side B. 1. Plat
13. Logan City Surv.

Sta	RR on grade	Ele	HI
6		493.560	
0+10		498.90	
		498845	
0	3.255	502.100 on stone	
0+10	3.200 on grade		
0+25	3.333		
0+50	3.555		
0+75	3.777		
1	3.999		
1+25	4.221		
1+50	4.443		
1+75	4.665		
2	4.887		
2+25	5.109		
2+50	5.331		
2+75	5.553		

498.845
3.255
502.100 Remark

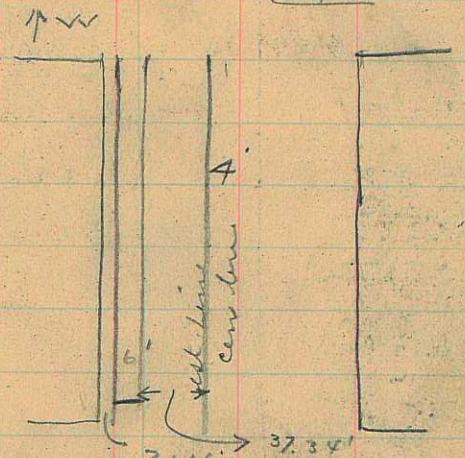
2 6 2.16 8.66

o/o = 0.89 per 100

502.100
498.90
03.20

at NW cor. B. 1. Plat B.

99



calc

2 (99
49.5
49.5
8.66
96.84

4 (89.0
.222

.0089
15
445
89
1335

2.16
6
37.34
4550
44.50

3

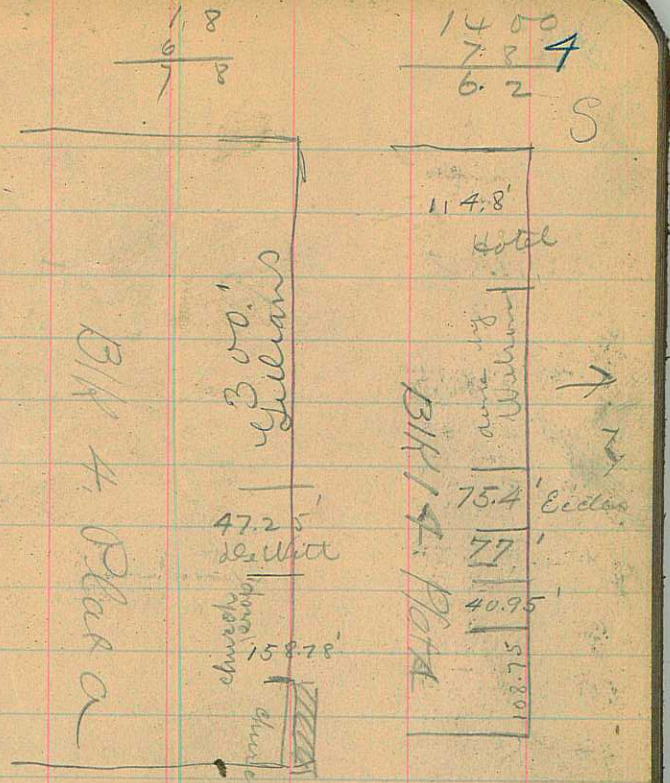
1 to RR

	on gr.
2.70	5.553
	.222
3	5.775
TP	.222
3+25	5.997
3+25	2.845
	.222
3+50	3.067
	.222
3+75	3.289
	.222
4	3.511
	.222
4+25	3.733
	.222
4+50	3.955
	.222
4+75	4.177
	.222
5	4.399
	.222
5+25	4.621
	.222
5+50	4.843
	.222
5+75	5.065
	.222
6	5.287

202.80 (5280

15840 38

44400



1 8
6
7 8

1400
7 2 4
6 2

S

N

30 | 5 2 8 0 | 30

2 0 7
2 2 7
2 1 0
1 7 8

1 7 6
3 0
5 2 8 0

202.80 (5280
8 4 0
3 | 6 9 0
2
3.3 8 0 0
2 0 2 8 0 0

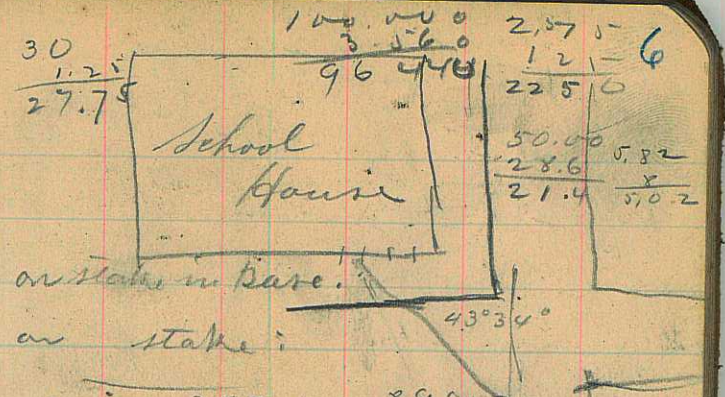
5 Drains for Central School at Preston Oct 4/04

Sta	BS	FS	Ele	HI
0	11.615		100.	
2+28.6		3.720		
2+28.6	1.560			
8+90		3.770		
8+90	1.740			
11+38	14.915	10.985	96.440	in creek.

18.475
14.915
3.560

0/0 = .312

Sta	RR on Grade	RR on ground	Cut into 0	Cut in "	HI
11+38	10.980	9.93	1.05	12 5/8"	107.420
	.118				
11	10.862	8.15	2.71	2' 8 1/2"	
	.156				
10+50	10.706	5.93	4.78	4' 9 1/2"	
	.156				
10	10.550	4.10	6.45	6' 5 1/2"	
	.156				
9+50	10.394	3.00	7.39	7' 4 1/2"	
	.083				
9+23.5	10.311	2.75	7.56	7' 7"	
	.103				
TP 8+90	10.208	2.583	7.625	7'-7"	



Sta	RR on grade	RR on Level	Cut in the	cut in
8+90	11.905	4.280	7.625	
	.125			
8+50	11.780	4.63	7.15	7' 1¾"
	.156			
8	11.624	5.78	5.84	5' 10"
	.156			
7+50	11.468	6.72	4.74	4' 9"
	.156			
7	11.312	6.71	4.60	4' 7¼"
	.156			
6+50	11.156	5.65	5.51	5' 6"
	.156			
6	11.000	5.03	5.97	5' 11½"
	.156			
5+50	10.844	4.58	6.26	6' 3"
	.156			
5	10.688	4.50	6.19	6' 2¼"
	.156			
4+50	10.532	5.03	5.50	5' 6"
	.156			
4	10.376	3.80	6.57	6' 7"
	.156			
3+50	10.220	3.20	7.02	7' ¼"
	.156			
3	10.064	2.20	8.44	8' 5½"
	.156			
2+50	9.908	1.80	8.11	8' 1¼"
	.067			
2+P +28.6	9.841	1.965	7.876	7' 10½"
		4.020		
2+28.6	11.896			
	.089			
2	11.807	4.32	7.49	7' 6"
	.156			
1+50	11.651	4.69	6.96	6' 11½"
	.156			
1	11.495	4.59	6.90	6' 10¾"
	.156			
	11.339			

HI 109,117

111,175

Ele on cent 7.625 / 4.286

104.837 11.905
104.49 11.78
103.34 11.62
102.406 11.468
102.415 11.46
103.47 11.31
104.09 11.00
104.54 10.844
104.62 10.688
104.69 10.532
105.32 10.376
105.92 10.220
106.92 10.064
107.32 9.908
107.155 9.841
106.85
106.48
106.58

1 138
890
248

10.980
777
10 203

11.62
5.78
5.84

11.46
6.72
4.74

11.31
6.71
4.60

11.00
5.03
5.97

10.844
4.58
6.26

10.688
4.50
6.19

10.532
5.03
5.50

10.376
3.80
6.57

10.220
3.20
7.02

10.064
2.20
7.84

9.908
1.80
8.11

9.841
1.965
7.876

11.807
4.32
7.49

11.651
4.69
6.96

11.495
4.59
6.90

8

00.312
248
2496
1248
624
.77774

00312
40
.12480

.312
21.4
1248
312
624
.066763

+ 250
228.6
21.4

.312
286
1872
2496
624
.089232

9

Sta	RR Grade	RR Grade	Cut	Cut	H I	Ele on contour
0+50	11.33	1.71	9.63	9'7 ÷ 2	111.175	109.46
0	11.183					

O K

11.20

11.34
1.71
9.63
12
126
63
7.56

50 ÷ 10
2
20 (16)
20 (13)
80 16

Note. 10/18/04

Look up for. No 11 in lot 5
Block 47. Plat "a" Logan
also lot 6,

Tract No 8 B.S. Plat a.
lot 3.

Tract no 12. B.S. " "
Lot 5 + 6

~~Tract No. B.S.~~ Plat a
~~lot~~

11 5.12
4.90

Independent work

4.90
4.64
.26

RR
4.64 in st cross. .32
Chas 4.83 on cor. S E.

5.85
4.83
.718
÷3
.239

6.585
2.154
4.431

Oct. 19/04
Grade for Jas E. Walsh Jr

Sta	RR	Ele	HI	BS.	FS
	3.238	100			
+P					
0	4.804				
5+99				2.115	
chas					
0	6.585				
2	1.436				
	5.149				
	.179				
2+25	4.970				
	.179				
2+50	4.791				
	.179				
2+75	4.612				
	.179				
	4.433				
3					

on mipes E 100 6.418

Sent Cty Eng to office 1/10/06

4.54
.18
4.36

12

Blk 12, Pl. D. Logan. 9th

sidewalk is placed 1.85 S of property line on N side of st between 1+2 E on 2 S.
(len = 599').
on grade SW cor. B. 12
on grade SE cor. B. 12

.07.0 = 0.718
2
1.436

6.418
2.115
4.303
4193
.1100
599
5010
4792
218

4)718
.179

599
.0718
4792
559
4192
42.9682

11 5.12 / 4.90

unadjusted work

4.90
4.64
.26

RR.
4.64 in st cross. .32
Chag 4.83 on cor. S E.

5.55
4.83

.718
.3
2.154

6.585
2.154
4.431

Det values

4.54
.18
4.36

12

13

Preliminary Sur of a canal Oct 27
Turner Canal Co.
Gentile Valley

Sta	BS	FS	Elev	HI	Rem
TP 0	3.814	3.314	100.00		on bluff on a knob surrounded with rock
	7.070	6.995			
	2.780	7.550			
	3.633	3.820			
	8.962	3.594			
	10.495	7.643			
	2.300	5.27			
39+70			4.895		on a large rock mount of Rocks
	7.850	5.027			
	7.528	5.675			
	7.075	1.962			
	4.305	9.620	1.025		where country is very rough on large rock near ground
	8.840	4.838			
	5.640	8.814			
60+75	6.500	4.804	107.136		BM on cedar stump
	7.115	4.885			

3.984
3.291
6.068

14

Remark

3.70
3.27
5.17

15 P. Lin of E Turner
con.
Oct 26/04

Sta	BS.	FS	Ele	HI.	Rm
60+75		4.804	107.136		
	6.500		107.136	113.636	
		4.885	108.751		
	7.115			115.866	
			110.71		
		6.346	109.520		
0	4.73		1	114.250	
0+30 +P		9.635	104.615		
0+30	4.45				
		4.45			
0+30					
2					

6350
0017
6350
10.79.50

6.50
4.88
1.62

107.136
6.500
113.636
4.885
108.751
7.115
115.866
109.520
6.346

104.615
4.91

Remark

{ Len of siphon 1024'

Len. of canal proper along E side of canon. 6350 ft 600 ft this is fluming. ofo of grade = 0.15

Sta 63+50 is where siphon empties and is on E end of canon. Sta 0 was began here to W across canon.

Δ E +	Δ -	RR	H I	Remarks
				on hub W side C
9	18.31			
4	15.53			

see over

17

Leveling at Springs
Oct 26/04

Sta	BS	FS	Ele 141
	6.730		on lowest Spring
	0.370	11.410	
	1.055	11.385	
	0.130	11.975	
	8.285	9.250	
		44025	
		8.285	
		35.740	

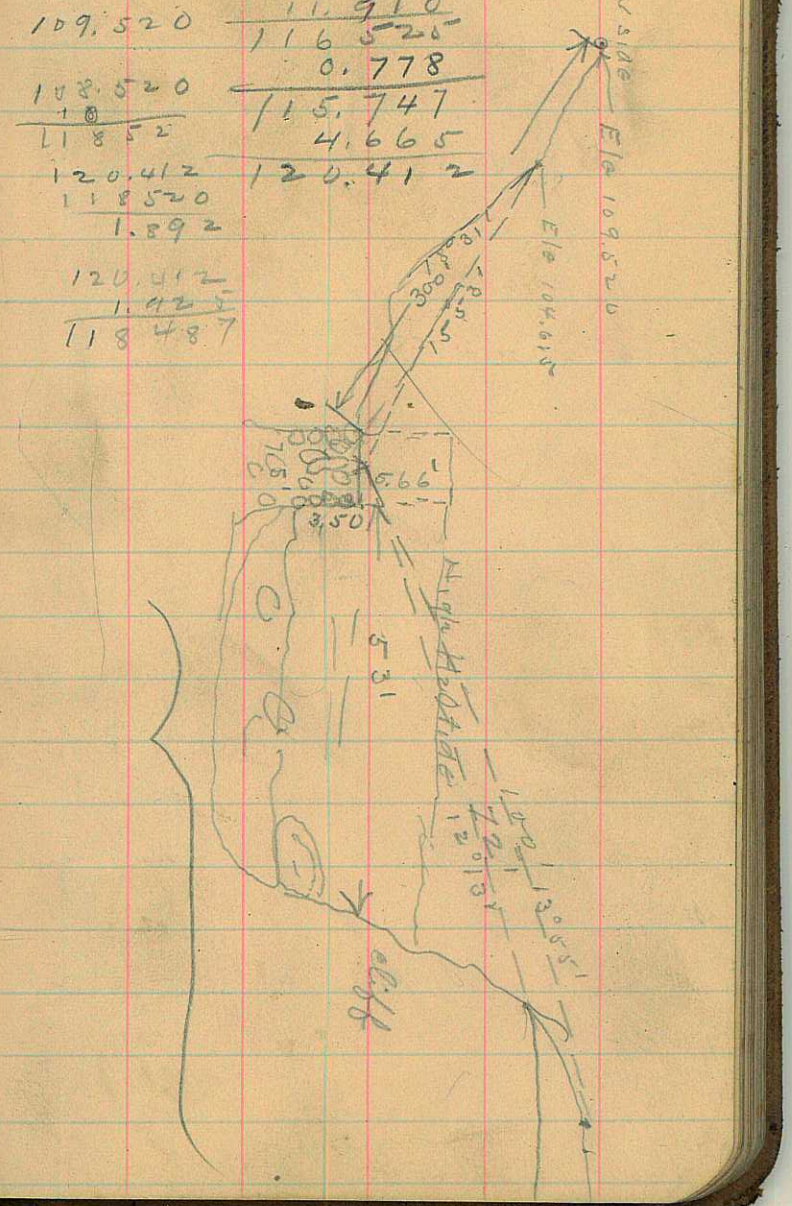
Syphon work
con. from Page X

11.91	0.778	104.615	116.525
	0.778	115.747	
4.665		120.412	
10+24	1.925	118.487	
		119.00	

104 — 2° 50'

109.520	104.615	
	11.910	
	116.525	
108.520	0.778	
10	115.747	
11852	4.665	
120.412	120.412	
118520		
1.892		
120.412		
1.925		
118487		

18



19 S. Turner

Sec. 33, 28 & 21

T p. 10 S. R 40 E

of Boise Mer.

Note Stadia indexes

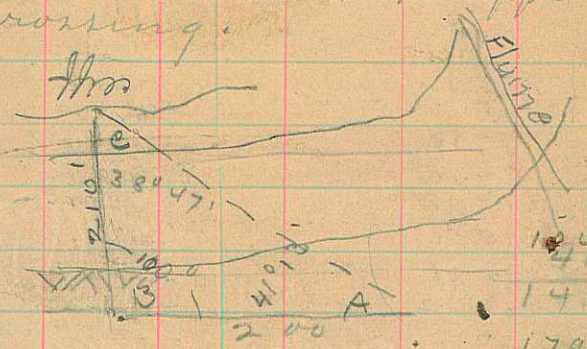
1' in 100.20.0'

Oct 27/04

99 | 12
26 | 14
73

P 64 0.6 64 83 20
6248 21 6589
6264

Dam Sur. at pt. between lower & upper crossing.



100 41.13
14113
179.60
141.13
3847

$\triangle CB'A \sim \triangle BA'C$

$\sin 41^\circ 13' = .6589$

200
131.78 00

131.78 | .6264
12528 | 2.10
6500
6264
2360

Measuring Depth of River

H I = 4.39

Ls = 29° 58'

Staria in. = 2(4.39 − 5.01)

Dist Sur to H2O = 57.45 from crest of Dam

Depth of Water, V. V = ? per Bed of River = 100'

Profile work

of S side Blk 17, Plat a Logan addn

Sta	H.I.	B.S.	F.S.	Elev	H.I.
℄		5.362		100	
℄		5.363		100.363	
	5.35			100.01	
	4.60			100.76	
0	5.30			100.06	
0+25	5.18			100.18	
0+50	4.91			100.45	
0+50	3.32			102.04	
0+75	4.80			100.56	
1	4.68			100.68	
1	2.15			103.21	
1+25	3.82			101.54	
+P.I 1+50			1.860	103.503	
1+50		11.330			114.833
1+75	8.27			106.56	
1+75	10.27			104.56	
2	5.55			109.28	
2	6.62			108.21	
2+25	5.50			109.33	
2+25	2.99			111.84	
2+50	2.87			111.96	
+P.I 2+50			0.990	113.843	
2+50		8.350			122.193
2+75	7.05			115.14	
3	7.80			114.39	
3	6.00			116.19	
3	8.85			115.34	
3+25	5.11			117.08	
3+50	4.67			117.52	
3+75	4.19			118.00	
3+75	5.79			116.40	

(over)

Remarks

(Width of 1st E on Nsid. 1st N = 98.7'

(Cen. of Blk 17 on S side = 5-99'

Blk 18

in cen. of cement walk at SE cor. of

in cen. of st. N side 1st N on 1st E.

in cen of st. where 1st E & 1st N intersects

on grnna cen. of walk. SW cor. Blk 17

" " " " " "

" " " " " "

in cen. of st.

on grnna cen. of walk

" " " " "

in cen. of st.

in cen. of walk

in " " " "

" " " "

in Bot of ditch

in cen. of walk

in cen of st.

in Bot of ditch

in cen. of walk.

" " "

in Bot of ditch

in cen of walk

" " " "

" " " "

in Bot of ditch

in cen. of walk

in cen of st

in cen of walk

" " " "

" " " "

in Bot of ditch

Sta	I M	B S.	F S	Elev	
3+75	4.15			118.04	130.11
4	3.63			118.56	
4+25	3.36			118.83	
4+50	2.74			119.47	
4+75	4.69			117.50	
4+50	1.50			120.69	✓
TP 4+75	1.[illegible]		1.825	120.368	
4.75		9.060			129.428
5+01.3	7.54			122.088	
5+[illegible]	11.[illegible]8			118.35	
5+18.47	6.88			122.55	
	6.39			123.04	
5+50	5.50			123.93	
5+[illegible]50	5.160			124.27	
5+57.9	5.048			124.38	
5+99	3.11			126.32	
	0.00			129.43	
TP 5+85.4			1.364	128.064	
5+85.4		6.68			134.744
	7.97	7.97		126.77	
			1.835	133.709	

Remarks

5.99 1.35 5.54 — 7.97

In cen of st.
" " " walk
" " " "
" " " "
in Bot of ditch
in cen. of st.
in cen of walk

" " " "
on N end of foot Bridge.
in cen of Bot. canal. Tryon & Dyckman
on E end. foot Bridge.
in cen. on N side large Bridge
in cen of walk at W side of Champs
on W side cement walk to champ house
" E side " " " " " "
in cen. of walk at SE cor B.17
in cen of 2 E of N side 1st N.

on Top of post N of SE cor B. 17
" " " "
In cen of 1st N of W side 2 E
Bam on N end of side at transformer house

Nov. 1/04

grade for. T. Thompson

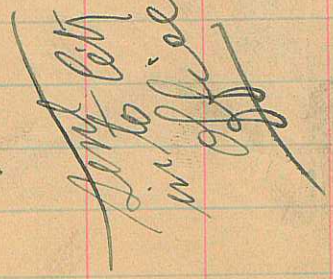
Sta.	RR	BS.	FS	Ele	HI
0		5.000			
		5.000			
0+98			10.75		
2+15.5			9.05		
3+13.5			1.70		

grade for. R. Murdock.

Nov. 2/04

Sta	RR	BS	FS.	Ele
	4.525	4.525		
	4.47			
0 TP			5.18	
0			3.950	
			6.970	
3+32.4	5.618			

at Murdock small gate



Remarks

grade = 4.200/0

on inside intersection of curb

4.47 + 5 = 7.97

4.81 − 4.52 = .29

4.81 − 5.10

Cen of BIK. 1 on S side where Murdock bldg = 600.81

on cen. N & cor BIK. 19 in of M. of N side 2 M.

(on grade at Eccles cor. inside Elevation

on grade SW cor min. Block of 0 = 0.502

6.970
3.950
3.020 (600.8
3.000.4000 .502
1 6000
1 2016

332.4
.00502
6648
16620
1.668648

3.950
1.668
5.618

27

Grade for Fleming
Nov. 3/04

Sta.	B.S.	F.S.	Elev.	H.I.
	7.545		100.00	107.545
		1.805	105.740	
	9.958			115.698
2+442	17.503	1.105	114.593	
2+442			111.820	

107.545
1.805
105.740
9.958
115.698
1.105
114.593

on cement at Fleming.

{on pivot in Gate post at Fleming.
on grade

2.50 2.38
5.8
2442

29 Surv. of Pipe line for Utah Con. milk factory Nov. 30/04

Sta	IH	BS	FS	Ele	HI	Remarks
0		6.15		300.0	306.15	On water at spring.
0	6.56	6.56		299.59		on cement wall N side of Catch B.
0+50	5.13			301.02		on ground.
1	11.11			295.04		" "
TP 1	10.670		10.670	295.480		on stake
1		1.06		296.540		" "
1+50	4.05			292.49		on ground
2	5.80			290.74		
2+50	7.33			289.21		
3	9.70			286.84		
3+24 TP			10.725	285.815		on stake
3+24		0.92		286.735		" "
3+24	4.27			282.46		on pipe at valves
3+50	3.00			283.73		on ground
3+50	5.12			281.61		in bot of trench
4	8.09			278.64		on ground
4	10.11			276.62		in bot of trench
TP 4			7.74	278.995		on stake

D K 2 50 ft 3.2 4 30

Sta	I.M.	B.S.	F.S.	Elev. H.I.	Remarks
4		0.33		279.325	on stake
4+50	5.94		273.38		on ground
4+50	7.58		271.74		in bot of trench
5	10.05		269.27		on ground
5	12.50		266.82		in B of T
TP 5			9.785	269.540	on stake
5		1.265		270.805	" "
5+50	7.22		263.58		on g.
5+50	9.50		261.30		in bot of T
6	11.91		258.89		on ground at Road trench
TP 6			11.400	259.405	on stake
6		1.140		260.545	" "
6+50	4.90		255.64		on ground
6+50	7.00		253.54		in B of T
7	7.81		252.73		on g.
7	10.12		250.42		~~on~~ T.
7+50	10.76		249.78		on g.
7+50	13.00		247.54		in T.
TP 7+50			10.410	250.135	on S.
7+50		0.000		250.135	
8	4.23		245.90		on g.
8	7.07		243.06		in T
8+50	7.63		242.50		on g.
8+50	9.90		240.23		in T
9	9.93		240.20		on g.
9	11.56		238.63		in T
9+50	10.01		240.12		on g.
9+50	12.10		238.03		in T
10	10.48		239.65		on g.
TP 10	12.90		237.23		in T
10			9.685	240.455	on S.

(over)

12.90
11.50
1.40

10.48
9.93
.55

Not T = trench
g = ground
S = stake

33

Pipe Surv. con. 11/30/04

Sta	HI	BS.	FS	Ele	HI	Remarks
10		1.270			241.725	
10+50	2.390			239.33		
10+50	5.12			236.60		
11	4.43			237.29		
11	7.30			234.42		
11+50	6.92			234.80		
11+50	9.52			232.20		
12	9.71			232.01		
12	12.30			229.42		
12+50	11.00			230.72		
12+50	14.00			227.72		
TP 12+50			10.570	231.155		
12+50		0.480			231.635	
13	3.34			228.29		
13	5.81			225.82		
13+50	4.98			226.65		
13+50	7.45			224.18		
14	8.62			223.01		
14	10.88			220.75		
14+50	11.00			220.63		
14+50	13.75			217.88		
TP 14+50			10.260	221.375		
14+50		2.370			223.745	
15	7.81			215.93		
15	10.73			213.01		
TP 15			7.075	216.670		
15		2.01			218.680	
15+50	9.17			209.51		
15+50	11.88			206.80		
16	12.40			206.28		
16	14.00			204.68		
16.50	11.90			206.78		
16+50	14.90			203.78		
TP 16+50			11.130	207.550		

Iron stake
on g
on T
on g
on T
on g
on T
on g
on T
on S
on S
on g
on T
on g
on T
on g
on T
on S
on S
on g
on T
on S
on S
on g
on T
on g
on T
on g
on T
on S

34

236.60
234.42
2.18
237.23
236.60
3.05

hollow

35

Pulse Aux Cor

11/20/64

Sta	HC	BS.	FS	Ele	HI
16+50		0.060			207.610
17	2.71			204.90	
17	5.32			202.29	
17+50	4.90			202.71	
17+50	7.21			200.40	
18	6.78			201.83	
18	8.81			198.80	
18+50	9.25			198.36	
18+50	12.10			195.51	
TP 18+50			8.700	198.910	
18+50		0.070			198.98
19	2.93			196.05	
19	6.09			192.89	
19+50	6.25			192.73	
19+50	8.30			190.68	
20	8.11			190.87	
20	10.98			188.00	
20+50	12.63			186.35	
20+50	15.13			183.85	
TP 20+50	12.[illegible]		12.13	186.850	
20+50		2.85			189.700
21	10.31			179.39	
21	12.75			176.95	
TP 21			9.520	180.180	
21		0.000			180.180
21+50	3.92			176.26	
21+50	5.90			174.28	
22	5.40			174.78	
22	7.88			172.30	
22+50	6.12			173.06	
22+50	8.55			171.63	
23	6.54			173.64	
23	9.88			170.30	
23+50	8.01			172.17	
23+50	10.93			169.25	

on S
on 9
on T
on 9
on T
on 9
on T
on 9
on T
on S
on S
on 9
on T
on 9
on T
on 9
on T
on 9
on T
on S

176.26
174.78
1.48

174.78
173.06
1.72

36

37

Pipe Ln cm
11/80/64

Sta	IM	BS	FS	Elv	HI
24	10.45			169.73	
24	12.75			167.43	
TP 24			9.790	170.390	
24		1.53			171.92
24+50	6.39			165.53	
24+50	9.18			162.74	
25	8.70			163.22	
25	11.30			160.62	
25+50	10.56			161.36	
25+50	13.00			158.92	
26	12.15			159.77	
26	15.15			156.77	
T 26			11.51	160.410	
26		1.500			161.910
26+50	5.40			156.51	
26+50	7.95			153.96	
27	6.66			155.25	
27	9.06			152.85	
27+50	7.80			154.11	
27+50	10.09			151.82	
28	8.45			153.46	
28	10.99			150.92	
28+50	10.30			151.61	
28+50	12.80			149.11	
TP 28+50			9.705	152.205	
28+50		1.850			154.055
29	4.40			149.65	
29	7.64			146.91	
29+50	6.68			147.37	
29+50	9.19			144.86	
30	8.61			145.44	
30	10.97			143.08	
30+50	11.50			142.55	
30+50	14.50			139.55	
30+50			11.04	143.015	

on 9
on T
on S
on 9
on T

on S

on 9
on T

to end of trench

1200
2

300.05
143.01
56.99
159.77
156.51
3.26
156.51
155.25
1.26
155.25
154.11
1.14
153.46
151.64
1.82

38

39

Sta	RR	RR Cut	F	From Top of S
8	3.09			
10+50	9.49			
	D = 6.40			
8	3.09			
	2.56			
	5.65			
8+50	~~3.65~~ 2'			
~~8~~+50	~~5~~ 5.87			
	1.81			
9	7.68	5.68	2'	
8+50	3.39	5.92	0.3	1.83
9+50	~~5~~ 5.30	6.05		

Sta	BS.	FS	TP
	6.59		
	5.81		
		6.20	

40

9.49
5.87
2(3.62
1.81

5.92
7
5.22
3.39
1.83

7.54
5.68
1.86

9.50
7.54
1.96

7.54
9
6.64

6.64
5.89
1.25

5.30
6
5.90

a.9R

5.22

(Surv. of Old man Warren)
in ditch at Spr.
S side of lot

at Ho. Oway at Odells
at cor of Blk. ?

41

Contours of Reservoir site.

Smithfield City Water Works.

Sta	BS	FS	Inst	Elev	H I
0	2.71			100	102.71
		2.30			
		7.64			
a		3.71	99		
		4.71	98		
		5.71	97		
		6.71	96		
		7.71			
		8.71			
		9.11			
a	2.98			100.	
b		5.03			
c TP		8.05		95	
c	2.76				
d TP		5.95		97	
d	2.05				
e		9.19			

see over

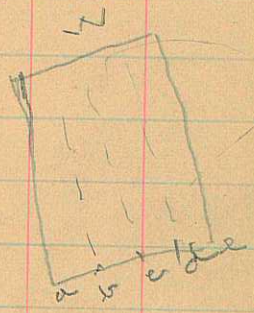
(con on page a)

42

7.64
3.71 102.71
3.93 99
3.71.

on SE cor of stake SE cor of site.
on map of stake in end of canal
(of SE cor)

On S line
11.7 W, 12.7 N W
24.6 N W, 28.6 SW,
61.3 SW
93.6 SW.
115 SW
140 SW
150 SW.



43

Mar 8/05 Grade run from The E side of the Res.

Sta.	H.I.	Actual H. above g.	R.R on ground	Cut.	
0	5.02	7.82		2.80	
0+50			4.63	3.19	
1			5.28	2.54	
1+50	change		4.96	2.86	✓
1+50	4.76	7.62		2.86	✓
2			4.97	2.65	✓
2+50			5.55	2.07	✓
3			5.15	2.47	✓
3+50			4.76	2.86	✓
3+82.5	change		4.65	2.97	✓
3+82.5	4.80	7.77		2.97	✓
4			4.80	2.97	✓
4+50			4.18	3.59	✓
5			4.60	3.77	✓
5+50			5.00	2.77	✓
6			4.61	3.16	✓
6+50			4.60	3.17	✓
7			4.13	2.84	
7+08	change		4.80	2.97	✓

Smithfield City 47

1+20 works.

Cut

4.76	4.76	7.82
2.86		4.63
7.62	7.82	3.19
	5.28	7.82
7.62	2.54	5.28
5.15	7.82	2.54
2.47	4.96	7.82
9.62	2.86	4.96
4.76	7.62	2.86
2.86	4.97	7.62
7.62	2.65	5.55
4.65		2.07
2.97	7.77	4.80
	4.18	2.97
7.77	3.59	7.77
4.61	7.77	4.80
3.16	4.60	2.97
7.77	3.17	
4.80		
2.97		

con on page 6

(a)

45

Sta	HI	RR	Dist W
b	4.80		
		3.62	25'
		6.02	50'
		6.75	75
		7.60	100
		9.08	125
		9.90	150
c	5.00		
		5.32	25'
		5.40	50'
		6.30	75
		7.51	100
		8.60	125
		9.18	150
d	4.95		
		5.65	25'
		7.00	50
		7.55	75
		6.90	100
		6.50	125
		7.00	150
e		7.85	150

Levels for Profile

on the West side of Block 17 Plat "A" Logan City

Nov. 27/05

76

Sta	BS.	FS	Int	Ele	HI	Remarks
				100.53		SW cor B.16 slope from Parallel N 0.5280/0
	4.470			99.93	104.40	on NE cor B. 2 on cement
			4.207	100.198		Sou SW cor. of intersection Lot SW cor. B.16
0			4.020	100.38		in cen. of 4' walk SW cor 16
1			4.525	99.875		" in cen of sidewalk in gr.
2			5.700	98.70		in cen of Street West
2			5.53	98.87		" " of walk
TP 3			6.150	98.25		
4		6.638	6.638	97.762		
4	2.750				100.512	
4			3.20	97.31		in cen of St. West
5			3.75	96.76		
5			4.00	96.51		Preston's on Lawn
5+24			3.90	96.61		on cement walk to Prestons House
600.1			4.57	96.94		NW cor B.16
600.1			4.66	96.85		in cent of St West
			4.87	95.64		on nail in Spout NE cor 15
			5.20	95.31		on ground NE cor 15
			5.12	95.39		on cen of cement SE cor B.18
0			5.22	95.22		SW cor B. 17 on ground
1			5.70	94.81		on sidewalk
2			6.05	94.46		in st West
2+50			5.25	95.26		in cent of sidewalk
3			5.05	95.46		
3		4.084		96.426		
3	9.097				105.523	
2+50			9.68	95.84		on Welkenmeir lawn
3			10.68	94.84		in cen of st. O
3+37			9.44	96.08		" " " "
3+44			7.32	98.20		Sou sidewalk app of Nebeker Bemart gate
3+50			6.35	99.17		on Nebekers lawn
3+50			6.94	98.53		
4			8.06	97.46		in Street
4+15			5.50	100.02		
4			3.82	101.70		at Bolis cement in Street
			1.43	98.09		

(b)

47

Sta.	+I	Actual RR on ground	RR on Cut		
7+08	4.98	7.95	2.97	✓	
7+50		5.05	2.90	✓	
8		4.73	3.22	✓	
8+50		3.38	4.57	✓	
8+94.4 Change		3.17	4.78	✓	
8+94.4	4.83	9.61	4.78	✓	
9+50			4.83	4.78	✓
10			4.90	4.71	✓
10+28 change			6.74	2.87	✓
10+28	4.93	7.80	2.87	✓	
10+50			3.28	4.52	✓
11			4.80	3.00	✓
11+50			4.93	2.87	✓
12			3.78	4.02	✓
12+52 change			4.92	2.88	✓
12+52	4.98	7.86	2.88	✓	
13			4.53	3.33	✓
13+58 change			4.87	2.99	✓
13+58	4.82		2.99	✓	

(Over)

7.80 4.93
4.92 2.87
2.88 7.80
4.98 3.28
7.86 4.52
4.87 7.80
2.99 4.80
3.06
7.80
3.78
4.02

7.95 7.95 4.88
5.05 4.73 2.97
2.90 3.22 7.95
7.95 7.95
3.17 3.38
4.78 4.57
4.83 9.61 =
4.78 4.90
9.61 4.71
9.61
6.74
2.87
7.86
4.53
3.33

{ From sta 10+28 to sta 13+58 slope of 1½ to 1 on R was the allowance of roadbed

Levels cor on W side B.17, Nov 27/05

Sta	BS.	FS	Inst Elev	HI	Remarks
4+50			5.00 100.52	105.52	in cor of roadway
4+50			7.06 98.46		in cor of st W
5			5.10 100.42		
6+04			6.40 99.12		mw cor B.17
			6.20 99.32		sw cor B. at Vernon
6+04			7.27 97.95		cor of st.

49

Sta to	HI	Actual RR on G.	RR on ground	Cut.	
13+58	4.82	7.81		2.99	✓
14			4.82	2.99	✓
14+50			4.82	2.99	✓
15			4.81	3.00	✓
15+50			4.81	3.00	✓
16			3.57	4.24	✓
16+41	change		3.52	4.29	✓
16+41	4.82	9.11		4.29	✓
17			6.31	2.80	✓
17+50			6.71	2.40	✓
18			6.70	2.41	✓
18+69			6.42	2.69	✓

Note

From Sta 18+69 to 24+30.6 an average cut of 2.50 ft. on steep incline down the road. from sta 24+30.6 to sta 28+80.6, (stakes marked A) cuts as shown on notes.

4.82	7.81	7.81	4.82
4.29	3.52	3.57	2.99
9.11	4.29	4.24	7.81
2.50			
6.61			
	9.11	9.11	9.11
	2.80	6.60	6.71
	6.31	2.50	2.40
	9.11	9.11	
	6.20	6.42	
	2.91	2.69	

Where trench goes onto Road from Sta 28+80.6 to E. line

51

Graded run
Through Geo Kinds
Hollow

Sta	BS	FS	HI	Cut
E	9.58			2.50
A		.00	grade	4.77
—		—		
		grade		
A		2.50	4.50	2.50 0
		2.38		
B		4.88		
		2.38	2.40	2.50 ✓
C		7.26	3.40	3.86 ✓
		2.38		
D		9.64	6.45	3.19 ✓
		2.38	✗	
E		12.02	9.08	2.50
		9		

E	2.62		act 5.12	RR on ground
U		6.68	9.18	2.50 ✓
I			8.38	3.46 4.92
H			7.58	3.00 4.55
G			6.78	4.00 2.78
F			5.98	3.68 2.80
			5.18	2.50

adjust 50

checked on paper
end of book

12.
9.08
12.02
9.08
2.94

7.26
3.40
3.86
9.64
6.45
3.19

9.58
8.00
1.58
1.40
.18
6.68
2.62
4.06

52
2.50
204.77
2.38
2.40
.33

All fish about 100 SW of bro of hall where long line changes

7.58
4.55
3.03

6.78
2.78

.8
5
4.0

5.98
2.50
3.68

4.06 | 2.50
2.50 | 2.01.60
1.56 0.80
1.50
0

7.38
4.92
2.46

6.68
2.50
9.18

8.38
4.92
3.46

53

Sta.	on grd. HI	HI	RR on gr.	Cut	
29+70	7.33	4.33		3.00	
30+70	+	4	4.33	3.00	
31+70	+		4.00	3.33	
32+70	+		4.55	2.88	✓
33+70	+		5.10	2.25	✓
34+70	✓		5.30	2.03	✓
35+70	+		4.83	2.50	✓
36+70	+		4.42	2.90	✓
37+70 +58	+		4.05	3.28	✓
38+28 +42	✓ reverse to E			2.50	✓
38+70	✓ 7.33		5.37	2.00	✓
~~39+70~~	✓ +		4.83	2.50	
40+70	✓ +		4.93	2.40	✓
41+70	✓ ✓		E	2.50	✓
42+70	✓ ✓				
43+70	✓ ✓				
44+70	✓ ✓				
45+70	✓				

10 deg. curve to the right

57

100 / .42 / 58

7.35 / 5.10 / 2.25

7.33 / 4.55 / 2.78

7.33 / 4.05 / 3.28

2.50 / 4.83 / 7.33 / 5.30 / 2.03

54

330 / 264 / 29+70

All that is marked 45 chs. on back of this. at Sta 14+00

7.33 / 5.70 / 1.63

3.828 / 442 / 42+70

7.33 / 2.90 / 4.43

7.33 / 5.70 / 1.63

7.33 / 2.30 / 5.00

7.33 / 4.42 / 2.91

Angles
∠ R

46+70
47+70
48+70
49+70
50+70
51+70
52+70
46
53+16

52+70
50
53+20
50
53+70
54+70
55+70
56+70 Start here
57+70
58+70

over

To E. line of SW¼ sec. 23.
{20° curve L. Def. 10°
Add Def. to PT.
on curve
PT ∠R 2°36'

no stake put in.
P.C. C.R 5°. Def 2°30'. 2 Def

P.T.

57

Sta	HI on grade	HI	RR.	Cut	
58+70	7.36	4.86		2.50	
59+20			4.86	2.50	
59+70			4.86	2.50	
60+20			—	—	
60+50			4.00	3.36	
61+00			4.96	2.40	
61+50			4.90	3.00	
62+00			3.65	4.24	
62+50			4.29	3.07	
62+50	7.89	4.82			
63+00			4.50	3.39	
63+50			4.82	3.07	
56+70	7.22	4.72		2.50	✓
57+20			3.45	3.77	✓
57+70			2.50	4.72	✓
58+00			4.60	2.62	✓

Remark

58

from this Sta I run up 34'

no stake in road

I run up 30'

no stake in road

4.86
2.50
9.36
4.30
3.06

7.36
4.29
3.07

7.89
3.65
4.24

7.89
4.90
2.99

7.89
4.50
3.39

7.22
3.45
3.77

7.22
2.50
4.72

7.22
4.60
2.62

59

Sta	HI on grd.	HI	RR.	Cut	
58+00	7.22	4.60		2.62	✓
58+50			3.00	4.20	✓
58+87			4.20	3.02	✓
59+37			4.33	2.90	✓
59+82			1.50	5.72	✓
60+11	change		4.66	2.56	✓
60+11	7.76	5.20			
60+51			2.50	5.26	✓
60+88			5.40	2.36	✓
61+38			3.50	4.26	✓
61+82			5.45	2.30	✓
62+32	change		3.67	4.09	✓
62+32	8.74	4.65	change	4.09	
62+82		change	2.55	6.19	✓
62+82	10.67	4.48		6.19	✓
63+32			8.17	2.50	✓
63+82			8.17	2.50	✓

8.88	5.20	7.22
1.04	2.56	2.20
9.92	7.76	60
	5.40	7.22
	2.36	4.33
	7.76	2.89
	2.50	7.22
	5.26	1.50
	7.76	5.72
	5.45	7.22
	2.31	4.66
	7.76	2.56
	3.50	7.76
	4.26	3.67
	4.65	4.09
	4.09	
	8.74	8.74
	2.53	2.55
	6.21	6.19
		4.48
		10.67
		2.50
		8.17
		2.58

up 30'

Sta	HI onga.	HI	RR onga.	cut	
63+82 50	10.67		8.17	2.50	✓
64+32			7.71	2.96	✓
64+82 50			6.45	4.22	✓
65+26	change		4.26	6.41	✓
65+26 50	11.29	4.88		6.41	✓
65+76 50			8.29	3.00	✓
66+26 50			8.31	2.98	✓
66+76 50			8.09	3.20	✓
67+26 50			8.03	3.30	✓
67+76 50			8.80	2.50	✓
68+26 50			7.80	3.50	✓
68+76	change		8.70	2.59	✓
68+76 50	7.49	4.90		2.59	✓
69+26 50		4.95	4.95	2.54	✓
69+76 50			4.95	2.54	✓
70+26			4.85	2.64	✓
70+76 50			4.80	2.69	✓
71+26			4.90	2.60	✓

11.29 − 2.50 = 8.79
6.41 − 4.85 = 1.56
10.67 − 7.71 = 2.96
11.29 − 8.03 = 3.32
8.31 − 2.98 = 5.33
10.67 − 6.65 = 4.02
11.29 − 8.80 = 2.49
11.29 − 8.09 = 3.20
10.67 − 6.45 = 4.22
11.29 − 7.80 = 3.49
7.80 − 3.50 = 4.30
11.29 − 8.70 = 2.59
7.79 − 3.50 = 4.29
10.67 − 4.26 = 6.41

At W end of R of W, John Peterson

11.29 − 8.29 = 3.00
9.49 − 4.80 = 4.69
4.90 − 2.59 = 2.31
11.29 − 2.50 = 8.79
7.49 − 2.50 = 4.99
8.79 − 2.50 = 6.29
7.49 − 4.95 = 2.54
4.85 − 2.64 = 2.21

63

Sta	HI on gd.	HI	RR on g	cut	
71+26	7.44		4.90	2.60	✓
71+76	change		4.83	2.66	✓
71+76	7.38	4.72		2.66	✓
72+26		4.30		3.10	✓
72+76		4.85		2.53	✓
73+26		4.90		2.48	✓
73+76	7.51	4.85		2.66	✓
73+76		5.00		2.50	✓
74+26		5.00		2.51	✓
74+76	change	4.81		2.70	✓
74+76	7.47	4.77			
75+26	change		4.61	2.86	✓
75+26	2.56	4.70			
75+76		5.00		2.56	✓
76+26		5.00		2.56	✓
76+76		4.70		2.86	✓
77+26		4.10		3.46	✓
77+76		3.25		4.31	✓

64

4.85
2.66
7.51

7.56
3.25
4.31

In cell

7.47
4.83
2.66
4.72
7.38
2.50
4.88
7.38
4.80
3.08

7.38
4.81
4.51 2.53

4.81
2.70

7.38
4.90
2.48

4.77
2.70
7.47
2.80
4.67

7.51
2.50
5.01

7.56 7.47
4.10 4.61
3.46 2.86
4.70
7.56
2.50
5.06

Where R. of May goes in Sewer
Land of Peter

65

4.00

	HI on gd.	HI	RR on RP	Cut	
78+26	7.56		4.00	3.56	✓
78+76	change		5.10	2.46	
78.76	7.46	5.00			
79+26			2.61	4.85	✓
79+76	—	—		2.50	
80+26					
80+76					
81+10					
81+34					
81+56					

	BS	FS,	RR		
80+76	8.27	10.77		2.56	✓
	1.36	1.36			
81+10	6.91	9.41	5.80	3.61	✓
		.96			
81+34		8.45	4.85	3.60	✓
		88			
		737		2.57	✓

over ✓

8.00
8.76
24

7.56
5.10
2.46
7.46
2.61
4.85

66

up: 1°34'

understood as 2.50 on gage pt.

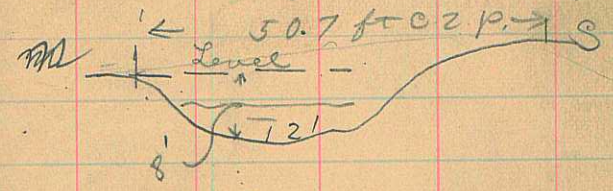
9.51
5.80
3.61

8.05
4.85
3.20

8.45

5.00
3.75
1.25

at mouth of siphon



Note; 1.50 fall across creek for siphon

Sta.	HI on gd.	HI	Cut
8+56 50.7			
82+06.7 65			
82+71.7 64			
83+35.7 64.3	9.78	4.78	5.00
84+00.0 50		6.80	2.98
84+50 83		7.20	2.58
85+33		7.28	2.50

Sta	angles L	R
.0		
0	56°28'	
1+94		4.33
4+16.1 4.51	66°38'	
8+67.1		4°09'
74+26	9°45'	
75+76	46°14'	
95.26		25°31'
94+76		29°23'
74 26		

17960
12332
5628

84000
8357
64.3

9.78
6.80
2.98

9.78
7.20
2.58

5.37
4.78
.59

4.78
2.50
7.28

9.78
2.50
7.28

5.37
2.50
7.87
2.00
19.87
4.78
5.09

322.1
316.1

68

Sta brow of hill 1+94' Rt
of each basin
up 32'

on Orig. ser.

" " "

going N on old ser

Where fence is.
Much same as sta 76+76 E of Res.

at fence

Sta	Angles L	Angles R
		29°23'
74+26		6°52'
73+76		3°34'
73+26		4°44'
72+76	27°12'	
72+26		5°08'
71+76		19°20'
71+26		19°02'
70+76		17°54'
70+26	28°22	
69+76	8°54'	
69+26	18°04'	
68+76	3°31	
68+26		14°48'
67+76	27°34'	
67+26		15°05'
66+76		3°27'
66+26		

{ which is 10.4' W of Elev of J.H. Petersen Creek

S 75° 38' W

Under Sta 66+26 the ending of the R of W

71

Level test on new inst. mar. 13/05

BS	FS	Elv	HI
5.771		100.00	605.771
	3.472		
6.417			
	1.783		
3.165			
	7.495		
3.3805			
18.733	5.981		
	18.731		

OK

12 / 14 / 26

99 / 26 / 73

16 / 180 / 144 / 37

72

at NW cor. B.15.

SW cor.

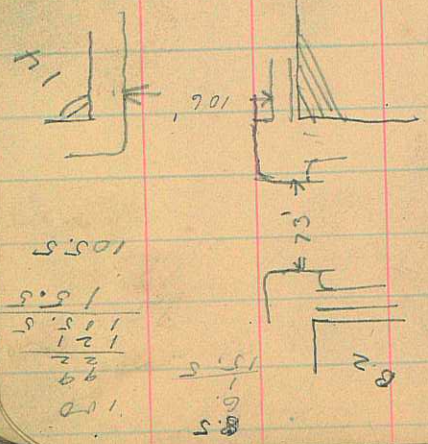
13

Sta RR

0 6.140
.250
5.890

164.5 | 121
93 | 93
71.5 | 28





14
02
.28

14/4 = 3.5 | 12
24 | .28
90

4.88 14
02
8

19

on curb. SE cor B.14

on " SW cor B.15

Mar 20 1900

BR. 4.88
28
4.60

on curb SW cor B.15
on inside Gr.

4.88
41
4.47 20' E

50 | 12
41
20

99
12
87
1.5
86.5

RR 6.32
30
6.02
.28
5.74

HI 4.787

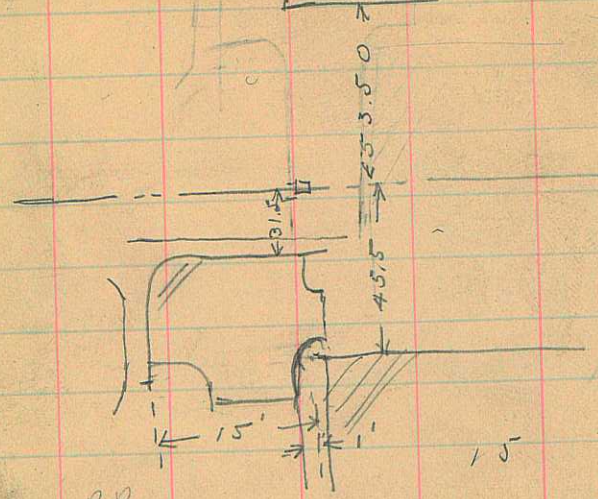
on curb N E cor B.14
on " mid cor. B.15
on inside Grade

1st N.

75

centerline

B. 18



RR

6.37
.30
6.07
.28
5.79

16.5
9
148.5
4
594.0

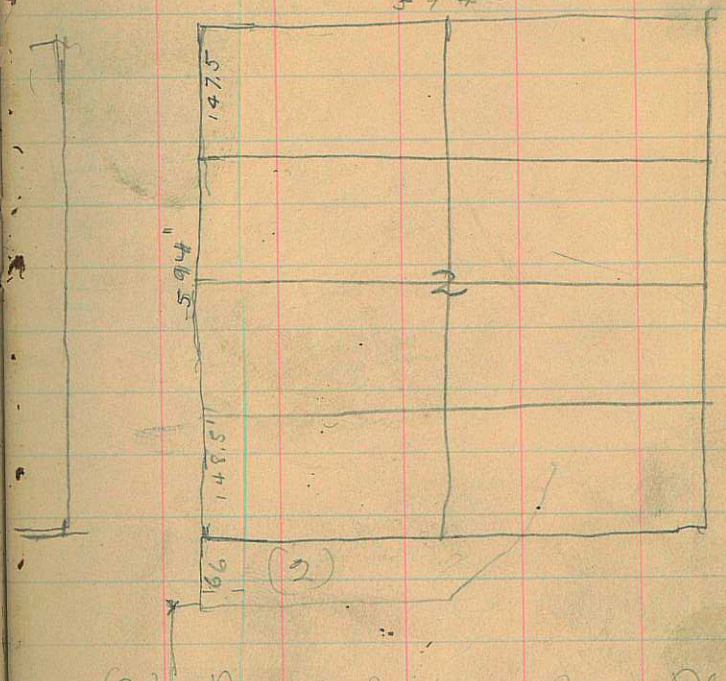
16.5
27
1155
330
4455

Surv. for City

16.5
36
990
495
5940

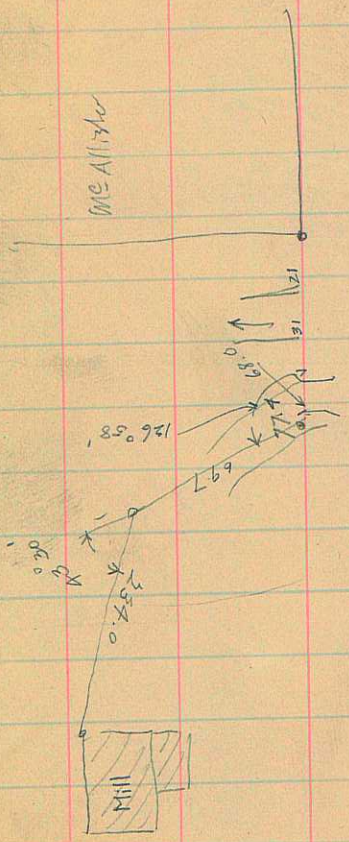
April 6/05
(PM)

76



(2) Beg at SW cor B 2, Plat to Logan City Surv. thence South 66 ft. East 237.6 ft. N E. 77.3 ft. W 278.3 ft. to beg.

77



5 | 261.3
5 2.6
2
1052

520
1578
264
3 | 23622
787.1/3
09
70.83

Blk 15

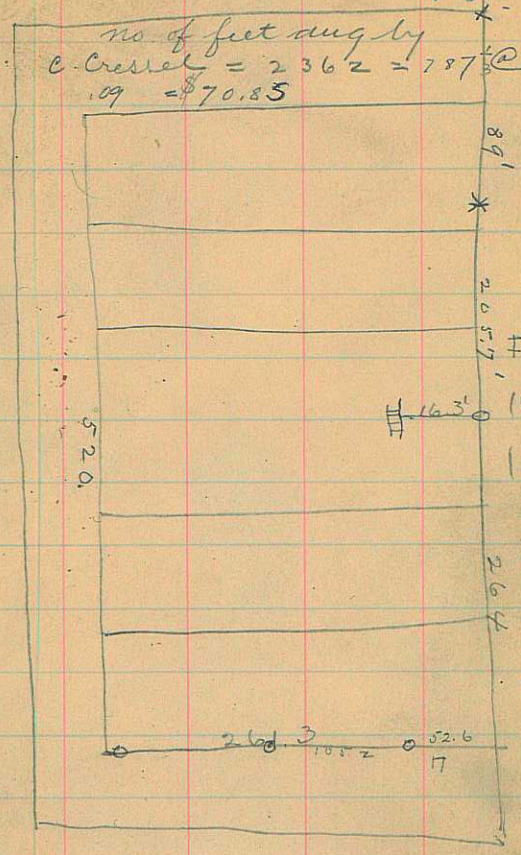
N.

263
1578

Main

78

no of feet dug by
C. Cresset = 2362 = 787 1/3 @
.09 = $70.85



198

79

Levels Johns A. Hendricks

april 9/05

	BS.	FS	HI
	4.124		
			4.160
			4.250
			4.34
TP		4.581	
	4.910	5.460	
	3.815		
		4.747	
	4.518		
TP		5.675	
	5.470		
	5.130	3.965	
		3.970	

80

On Riter's door sill.

On cement at Riter's door sill

On Cement Hendrick's S. line

On " near. Hendricks door,

On first floor line " near. cement Store

{could note go through Building

On first floor line Hendricks store.

at N.E cors B.14

" " " " "

on curb E side of lane

" " " " " " "

On floor West End of Hendricks. store

81

Levels at pipe line for Smithfield Ct.
April 8/05

Sta.	on gr. HI	cut	on g HI	fill
a	7.53			
b	7.25	0.28	at point	
b		change	7.08 / 23 / 7.36	
b	7.36			
b.	on g 6.72			
b	6.66	change		
X		.6.60	6.00	
X		-5.10		
X				7"
X				0
X		.5 4'	6.12	~~5 4~~
X	6.85	change		
4			6.64	

	BS	FS	Trunk line at Basin
0	6.76		
6+16.5	.45		L
50	7.21		
	.45		L
10	7.66		
	.45		4
11	8.11		
2	.8.56		

7.53 / 3.25 / .28

7.53 / 7.05 / .48

6.66 / 6.12 / .54

7.53 / 6.70 / .83

6.85 / 6.5 / .21

6.70 / 7.3 / 5 / 6.55 / 6.21 / .64

82

Angle — -30

7.08 / .36 / 6.72 / 1

{Where uniform grade ends on C. Str. 78+76 from R.

3.28 / 2.36 / 5,84

at Rocky point.

29'

on trench

83 April 8/05.

RR on first Sp. 5.10

" in bot of trench 6.76

Sta.	BS.	FS	HI	Ele	HI
0	5.28			112.26	117.54
0+25	~~5.30~~		5.30	112.24	
0+50			5.65	111.89	
0+75			5.59	111.95	
1			5.87	111.67	
1+25			6.25	111.29	
1+50			6.82	110.72	
1+75			7.42	110.12	
2			7.46	110.08	
2+25			7.51	110.03	
2+50			7.73	109.81	
2+75			7.70	109.84	
3			7.70	109.84	
3+25			7.62	109.92	
3+50			8.15	109.39	
3+75			8.20	109.34	
4		8.680		108.86	
4	3.4				112.26
4+25			3.61	108.65	
4+50			3.58	108.68	
4+75			3.44	108.82	
5			3.42	108.84	
5+25			3.85	108.41	
5+50			4.70	107.56	
5+75			5.39	106.87	
6			5.75	106.51	

3.57 3.53 4 — 3.71 3.53 .18

Remarks 89 3.53 1.42

78+76

{ Work goes the same as 15+1 going N on Rub in trench

Rocky point.

Sta	BS	FS	Inst	Ele	HI
6			5.75	106.51	112.26
6+25			5.40	106.86	
6+50			5.20	107.06	
6+75			5.14	107.07	
7			5.88	106.38	
7+25			5.87	106.39	
7+50			6.20	106.06	
7+75			6.25	106.01	
7+92			3.82	108.44	
8			6.58	105.68	
8+25			6.85	105.41	
8+50			6.75	105.51	
8+75			6.80	105.46	
9			7.30	104.96	
9+25			7.40	104.86	
9+50			7.95	104.31	
9+75			7.62	104.64	
10.00		7.950		104.31	
10.00	4.780				109.09
10+25			4.74	104.35	
10+50			5.08	104.01	
10+75			5.68	103.41	
11			5.57	103.52	
11+25			6.02	103.07	
11+50			6.27	102.82	
11+75			6.28	102.81	
12			6.76	102.33	
12+25			6.78	102.31	
12+50			7.28	101.81	
12+75			7.12	101.97	
13			7.55	101.54	
13+25		7	7.45	101.64	
13+50		7.49		101.60	
13+50	6.60				108.20

on a sub-sta 70+76

87

	BS	FS	HI Ele	HI
13+75			7.10	101.10 ✓ 108.20
14			7.95	100.25 ✓
14+25			8.20	100.00
14+50	—	—		
14+75				
15	—	—	8.20	100.00 ✓
				102.26
15		5.94	(on a hub)	

Levels on pipes in lab sq. April 11/05

5+20	5.40	
0+00		7.590
0+25		7.485
0+50		7.380
0+75		7.275
1		7.170
1+25		7.065
1+50		6.960
1+75		6.855
2		6.750
2+25		6.645

Over

.042 / 16 / 252 / 42 / .0672

.0042 / 12 / 84 / 42 / .00888

Our trench 63+82 which is 16.5 ft W of sta

at SW cor. B.15. on pipe run N & S. at NW cor going S.

89

Sta	B.S	FS	HI
2			6.75
2+12			.05 / 6.70 / .05 / 6.65
2+24			5 / 6.60
2+36			6.55
2+48			6.50
2+60			6.45
2+72			6.40
2+84			.05 / 6.35
2+96			6.30
3+08			6.25
3+20			6.20
3+32			6.15
3+44			6.10
3+56			6.05
3+68			6.00
3+80			5.95
3+92			5.90
4+04			5.85
4+16			5.80
4+28			5.75
4+40			

90

Sta	BS	FS	HI
4+40			5.75
4+52			5.70
4+64			5.65
4+76			5.60
4+88			5.55
5+00			5.50
5+12			5.45
		5.87	5.87
		5.65	6.11
		.22	5.87
			0.24
		0	5.65 on 2" pipe Sta
			.03 after rain
	0+12		5.62 going on
	0+24		5.74
	0+36		5.74
	0+48		5.78
	0+60		5.810

.220 | 80 / 160 / 600 / 00.27

.0047 / 27 / .1082

00,42 / 8 / .336 / 24 / .576

6.11 / .57 / 5.54

91

Final Grades in trench for Smithfield City Water works pipe April 12/05

Sta	BS.	FS	HI	RR. mt. Elev.	H I
0	4.590 .204			112.26	
0+25			4.794		
0+50			4.998		
0+75			5.202		
1			5.406		
1+25			5.610		
1+50			5.814		
1+75			6.018		
2			6.222		
2+25			6.426		
2+50			6.630		
2+75			6.834		
3			7.038		
3+25			7.242		
3+50			7.446		
3+75			7.650		
PP 4		7.854	7.850		

4.590 .817 2.451 3 7.041 2451

4.590 .817 5.407 4.817 .204

92

Remarks

Cut Grade 0.817 %

{ Which is same as sta 78 17+ C. of Res.

Rocky point

93

No	BS	FS	HI	RRemg.	Ele
4	4.230		4.230		
			.204		
4+25			4.434		
			.204		
4+50			4.638		
			.204		
4+75			4.842		4.40
			.204		
5			5.046		4.38
			.204		
5+25			5.250		4.80
			.204		
5+50			5.454		
			.408		
6			5.862		3.15
			.408		
6+50			6.270		
			.204		
6+75			6.474		6.03
			.204		
7+00			6.678		
			.204		
7+25			6.882		
			.204		
7+50			7.086		
			.204		
7+75			7.290		
			.204		
TP 8		7.494			
					105.774
8	4.660		4.660		
			.204		
8+25			4.864		

112.260
6.536
105.724
7.260
X 10384

1817
8
6536
10038
18844
111.94

6.47
6.03
.44

2(817
.408

99

5.86
3.15
2.71

cut

.425 = 5"

.06 = 8"

.45 = 5 11/16"

2.71. = 2'9" Where trench was moved

.44 = 5 7/16"

95

Sta	BS	FS	HI	RR or Ground Elev	HI	Cut. RR or Ground Contour	Remarks
8+25			4.864				
		.204					
8+50			5.068				
		.204					
8+75			5.272				
		.204					
9+00			5.476				
		.204					
9+25			5.680	2.80		2.80	trench moved 3' N.
		.204					
9+50			5.884				
		.204					
9+75			6.088				
		.204					
10+00			6.292				
		.204					
10+25			6.496	6.05		5"	
		.204					
10+50			6.700				
		.204					
10+75			6.904				
		.204					
11+00			7.108			4.50	
		.204					
11+25			7.312				
		.204					
11+50			7.516			4.40	
		.204					
11+75			7.720				
		.204					
12			7.924			5.60	
		204					
12+25			8.178				

5.68
2.60
3.08

96
5.68
2.80
2.88

Sta	BS	FS	HI	RR on T	Ele HI	Cut	RR on contour
12+25			8.178				
			204				
12+50			8.382 ✓				
			204				
12+75			8.586				
			204				
13			8.790				
			204				
13+25			8.994		8.70		
			204		8.520 TP.		
TP 13+50		9.198	9.198		8.70	3½"	5.78
							on stake driven
13.50	7.190		9.402			6"	3.00
	.678						
13+50	7.868		7.868 ✓				on stake driven
			204				
13+75			8.072		7.62		on gr.
			204			5½"	5.65
14			8.276 ✓				
			204				
14+25			8.480 ✓				5.80
			204				
14+50			8.684 ✓				
			204				
14+75			8.888 ✓				
			204				
15			9.092 ✓				4.50
			204				
15+25			9.296				
			204				
15+50			9.500		9.20		
			204				
15+75			9.704				6.90
							6.72
						3½"	7.60

9.19 − 8.70 = .49
8.99 − 8.70 = .29
8.58 − 5.65 = 2.93
8.07 − 7.62 = .45

9.198 − 8.520 = .678

4.590 + 4.250 + 4.660 + 7.868 = 21.348
6.810 + 9.198 + 7.494 + 7.854 = 31,366
31.34
10 026
112,260
140.026

Sta	BS.	FS	IM	RR or Cl.	HI
15+75			9.704		
			.204		
16			9.908	9.50	
			204		
TP 16+25			10.112	9.60	
16+25		9.540			
16+25	4.910				
	.572				
16+25	5.482		5.482		
			.204		
16+50			5.686		
			.204		
16+75			5.890	5.59	
			204		
17			6.094	5.59	
			.204		
17+25			6.298		
			.204		
17+50			6.502		
			.204		
17+75			6.706		
			.204		
18			6.910		
			204		
18+25			7.114		
			.204		
18+50			7.318		
			.204		
18+75			7.522		
			.204		
19			7.726		

6.09
5.58
.51

10.11
9.60
.51

100

10.112
9.540
.572

Cut	RR or contour
5"	
6"	5.20
on stake in trench	
" " " "	
on gr.	
	2.20
3½"	
6"	3.00
	2.60
	3.80
	3.20
	2.40
	4.20
	3.30
	3.53

101

Sta	BS.	FS.	IM	RR on T	Ele	∆	cut	RR on cur
19			7.726					
			204					
19+25			7.930					
			.204					
19+50			8.134					
			.204					
19+75			8.338					
			.204					
20			8.542					
			204					
20+25			8.746					
			.204					
20+50			8.950					
			204					
20+75			9.154					
			204		8.90			
21			9.358					
			204		8.70			
21+25			9.562					
			204		8.92			
21+50			9.766					
			204		9.21			
21+75			9.970					
			204		8.30			
22			10.174					
			204					
			10.378					

Note over

	5.70	
	6.15	
	6.25	
	6.20	
	4.90	
	6.10	
3"	6.10	
8"	4.80	
8"	5.50	
7"	6.10	
1'8"		

102

9.76
9.21
.55

9.97
8.30
1.67

9.36
8.70
.66

7.56
8.92
.64

11.20
11.70

Sta	BS	FS	HI
11	9.810		
10+50			9.45
10			6.20
9+25			7.20
9			6.08
8+50			5.30
8			4.80
7+50			4.50
7			4.15
6+50			3.25
6			4.40
5+50			3.50
5			2.60
4+50 TP			2.50
4		1.70	~~1.70~~
4	6.48		

Sall reading on old contour from Sta 11 and E.

11 here it was moved 3' N

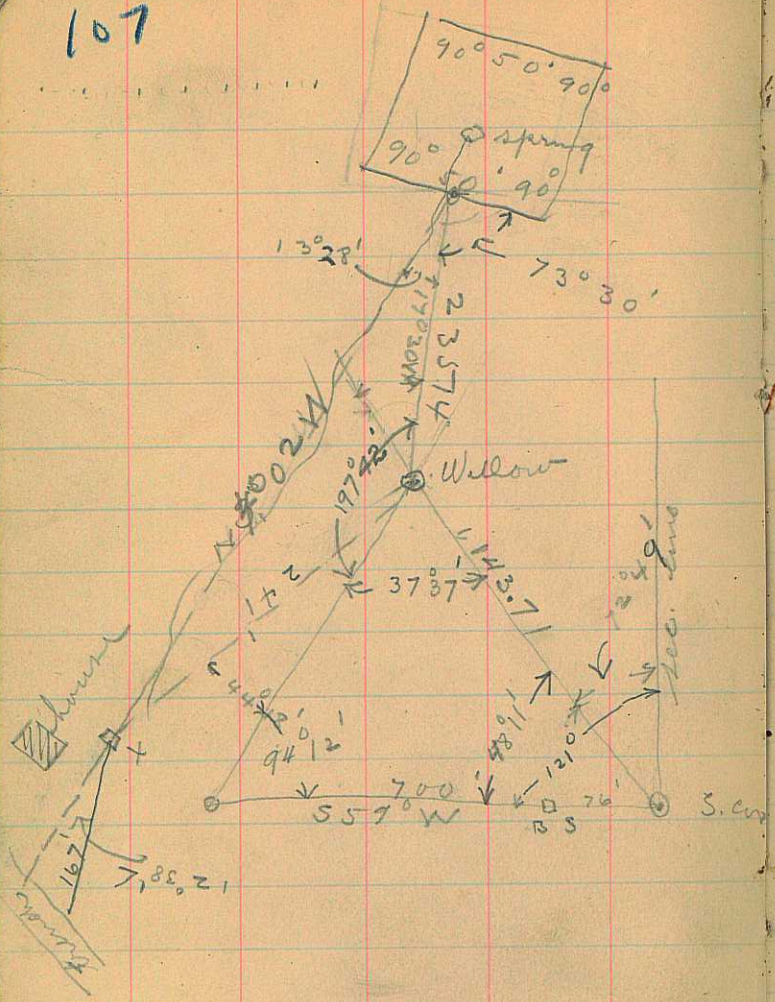
105

Sta	BS	FS	HI
4	6.48		
3+50			6.10
3			6.00
2+50			5.45
2			5.00
1+50			3.95
1			2.10
50			2.70
0			3.10
0		5.76	

on hub in street

89.60
89.02
106

107

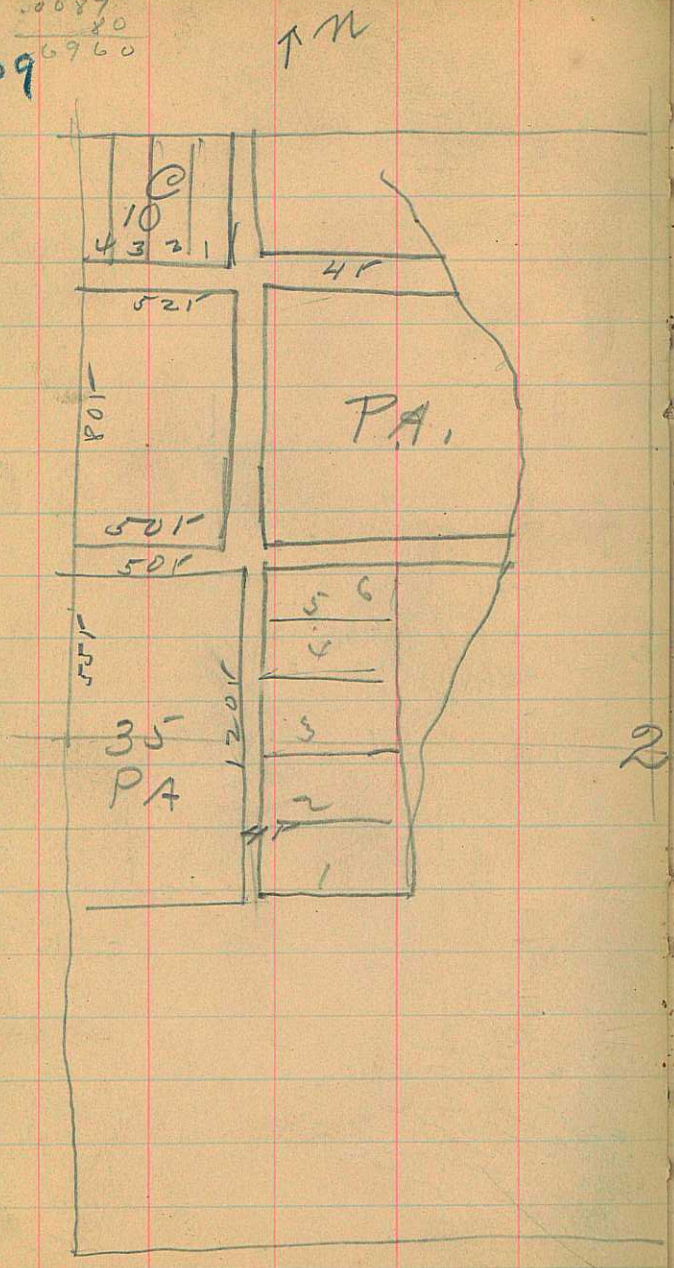


108

1 8
120 60'
7 2 49
4 11
3 7 37
8 5 48
1796
8548
9412

.0087
80
6960

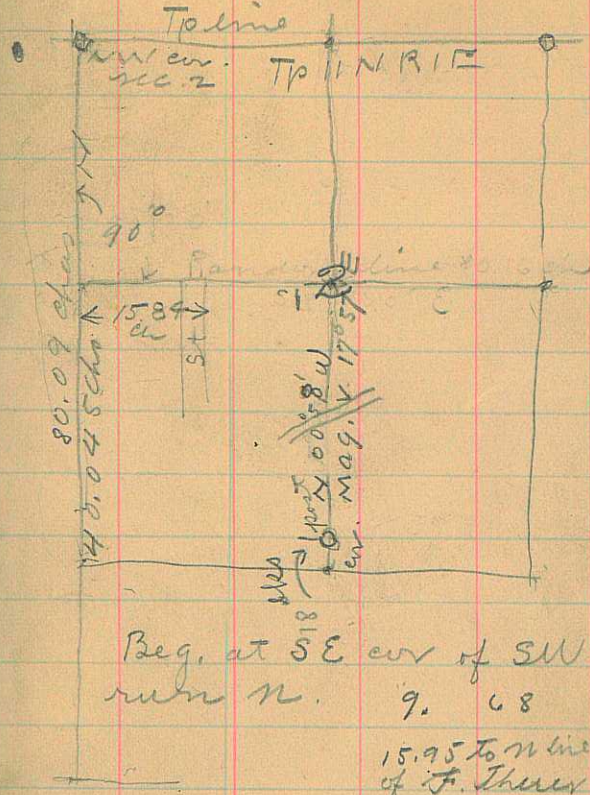
109

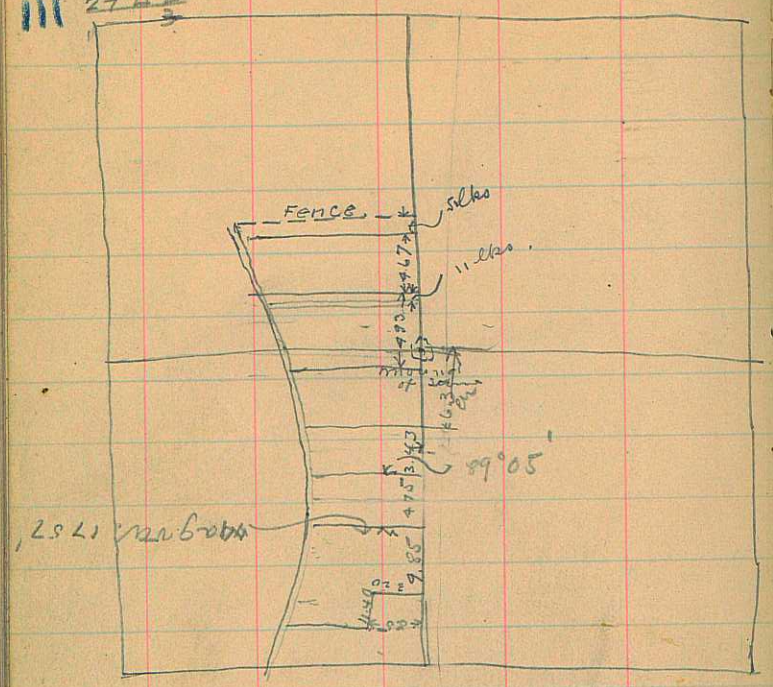


2

.0800
80

110





Sec. 2.

Hyrum Dist.

Mag. Var. 18° 15' E

Chas Rranzenberger
Des.

112

Beg at a pt, 14.48 chs S of NE cor of SW¼ sec.

2. S 9.85. W 3.20.

SWerly 11.40 to pt 8.60 chs N of ¼ line. (which bears S 27° 42' W. mag var 17° E.) N 80° W 4 chs to witness no C. Erly to pt W of beg E 9.25 chs to beg.

27° 42'

List of mound of stone from SE cor. of SW¼ is 40.32 chains

113

16
99
115

8.27
2.50
10 77

137
16
121
99
22

16
100
21
137

2 (99.00
49.50

49.5
4
53.5

49.00
53.50
455 0

49.0
2.25
66
1350
1350
1485 0

H 12" 7.45
2.01
.5

H 6" 472

L 5"

H 8"

H 8"

H 8"

H 8"

H 8"

12

0.86
6 22
.64

6.86
4 5
.44

845
676
1.39

676
.45
7.21

400
500
500

15.00

14.00

1500

114

66
.55
330
330
36.30

10.40
7.60
2.80

10.90
6.00
4.40

1.79601 2 need take
1320
36.3 104022
135 63 7538

6.90
5.60
1.30

.86
5
4.30

5.00
2
3.40

4480 6000
4200 .746
2800
4000

8.27
5.00
327

.746
2.80
59680
1492
2.08880

8.45 34
4.85 24
3.60 22
80

224
.88
104

3.27 .80
320 1074
7 34

6

5720 .24
2088 .104
3632 .96
75
4.382

34
.104
1.36

2

6	5	4	3	2	1
7	8	9	10	11	12
18	17	16	15	14	13
19	20	21	22	23	24
30	29	28	27	26	25
31	32	33	34	35	36

115

(X)

#	HI.	HI	R.R.	cut
E	7.32	4.82		2.50
A	7.32		4.82	2.50
B		(H 5" L 4	5.10	2.22
C		L 4	4.00	3.32
D		L 6" L 3" H 6" 0	4.70	2.62

BD.

5	00.00	5.71	Σ 19.65 = 1.29336
8.20	2.43	4.06	
7.49	.70	6.72	Σ .1703 = 3,23121
7.95	6.71	13.00	3 06215
8.68	8.40	29.49	
32.32	8.24	9.84	6.60
20.06	8.46	19.65	4.78
12.26	9.84	4.37	3.40
		15.28	5.28
		6.40	20.06
		21.68	

.0
.01154

3120.9
417.4
1,7035

	B.S.	F.S.	385'
	1.30	7.76	840
		1.30	403
		6.40	3.37

12.260 | 1500
12000.0081
2600
1500
1000

7.32 × 204.82 = 2.225

7.32 × 2.42 = 4.00 + 64

1.23

1.15

7.32 × 1°23
4.20
2.62

80.59
66
48344
48324
53784

9°42 = 116

60 540 542 582 540 420 360 60

180 3.2 180 540 720

830 | 500 .166 3300 3000 .166 50

50 3.2 100 150 160.060 120 40 2

5.50
5.70 on 6.1
5.50 5.7
0.4

(X)

	HI	HI	cut	RR	
J	7.34	4.84	2.50	4	3.63
E			2.50	4.84	7.34 3.32 4.02
F			3.63	3.71	7.34 4.30 3.04
G			4.00	3.32	7.34 3.95 3.39
H			3.00	4.30	
I			3.39	3.95	

2.640 reef

2½ reef

11.37 reef

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